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The surface modifications of multi-walled carbon nanotubes for multi-walled carbon nanotube/poly (ether ether ketone) composites

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Abstract

The effects of surface modifications of multi-walled carbon nanotubes (MWCNTs) on the morphology, dynamic mechanical and tribological properties of multi-walled carbon nanotube/poly (ether ether ketone) (MWCNT/PEEK) composites have been investigated. MWCNTs were treated with mixed acids to obtain acid-functionalized MWCNTs. Then the acid-functionalized MWCNTs were modified with ethanolamine (named e-MWCNTs). The MWCNT/PEEK composites were prepared by a solution-blending method. A more homogeneous distribution of e-MWCNTs within the composites was found with scanning electron microscopy. Dynamic mechanical analysis demonstrated a clear increase in the storage modulus of e-MWCNT/PEEK composites because of the improved interfacial adhesion strength between

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e-MWCNTs and PEEK. Furthermore, the presence of e-MWCNTs caused an enhancement in the glass transition temperature of the composites. Wear tests have shown that the friction coefficient of e-MWCNT/PEEK composites decreased significantly during the test after the running-in period. This suggests that there is an obvious improvement in tribological properties of e-MWCNT/PEEK composites. Overall, the e-MWCNT/PEEK composites have exhibited improved properties and are promising for their applications in industry.

Keywords: Surface modifications; composites; dynamic mechanical properties; tribological properties.

1. Introduction

Poly (ether ether ketone) (PEEK) is a high-performance semicrystalline thermoplastic polymer that displays a unique combination of thermal stability, low flammability, chemical resistance and excellent mechanical properties over a wide temperature range [1, 2]. This polymer has found a wide application since its commercialization, such as electronics, medicine, tele-communication and transportation industries (automobiles, aircraft and aerospace) [3]. However, it is difficult to use PEEK in pristine form because of its high friction coefficient and stick-slip behavior. Many research efforts have been devoted to a further improvement of the properties of PEEK via an incorporation with fillers, such as carbon fibers, glass fibers [4, 5], and nanoparticles [6–8].

Carbon nanotubes (CNTs) have attracted great interest in polymer reinforcement owing to their extremely high Young's modulus, strength and flexibility [9–11]. Achieving a good dispersion of CNTs in a polymer matrix is the key to fabricate composites with enhanced properties. However, this is commonly a difficult task because carbon nanotubes have a strong tendency to gather and form bundles. To improve the dispersibility of CNTs in polymer matrices, some strategies, such as dispersing CNTs in compatibilizing agents [12] or grafting functional groups onto CNTs' surfaces [13], have been employed. Many studies on the functionalization of CNTs and the synthesis of carbon nanotube and PEEK (CNT/PEEK) composites have been carried out since the last decade. Diez-Pascual et al. prepared single-walled carbon nanotube and PEEK (SWCNT/PEEK) composites incorporating polysulfones-I [2], polysulfones-II [14] and polyetherimide [15] as compatibilizers separately and investigated the thermal and dynamic mechanical properties of the SWCNT/PEEK composites. Song et al. worked with sandwich-like SWCNT paper/PEEK composites to study their mechanical performance [16]. Rong et al. studied the effect of multi-walled carbon nanotubes (MWCNTs) on the mechanical properties and crystallization behaviour of PEEK [17] and Ogasawara et al. researched the stress-strain behaviour of multi-walled carbon nanotube and PEEK (MWCNT/PEEK) composites [18]. These studies have been focused on the effects of different modified CNTs on morphological, thermal and mechanical performance of CNT/PEEK composites. However, few detailed reports can be found on the effects of MWCNTs' surface modifications on the dynamic mechanical and tribological properties of MWCNT/PEEK composites, which could make MWCNT/PEEK composites more suitable for a wide range of property requirements in applications.

The work reported in this paper was aimed at studying the effects of surface modifications of MWCNTs on compatibility between MWCNTs and PEEK as well as dynamic mechanical and tribological properties of MWCNT/PEEK composites systematically. The MWCNT/PEEK samples at an identical MWCNTs concentration of 4% were prepared by solution blending in an organic solvent named N,N-dimethylformamide (DMF). An extensive comparative characterization was carried out in order to evaluate the potential improvement in MWCNTs' dispersibility in PEEK matrix, the morphology, structures, dynamic mechanical and tribological properties of MWCNT/PEEK composites.

2. Materials and methods

2.1 Materials

PEEK 450G used in this study was provided in granule form by Jilin Zhongyan

High Performance Engineering Plastic Co., Ltd, China, with physical properties of density of 1.26 g/cm³ at 25°C, melting temperature of 343°C. Parent MWCNTs (p-MWCNTs), provided by Chengdu Institute of Organic Chemistry, China, had outer diameter of 30~50 nm, inner diameter of 5~12 nm, length of 10~20 μm and purity of 95%. Ethanolamine of 99% purity was purchased from Tianjin Fuyu Chemical Co., Ltd, China. N,N-Dicyclohexylcarbodiimide (DCC) of 99.5% purity was supplied by Aladdin Chemistry Co. Ltd. N,N-Dimethylformamide (DMF) of 99.5% purity was obtained from Tianjin Bodi Chemical Co., Ltd, China.

2.2 Surface modifications of MWCNTs

It is well known that the preparation process of MWCNT/polymer composites is hindered by the poor dispersibility of MWCNTs in polymer and their strong tendency to aggregate and form bundles. In this study, an acidic treatment on MWCNTs in mixed acids was employed to introduce oxygen-containing groups (hydroxyl groups and carboxyl groups) onto the surfaces of MWCNTs for the reactions with some specific functional groups, which could improve the dispersibility of MWCNTs in PEEK matrix. The purpose of further surface modification of MWCNTs by ethanolamine was to graft functional groups (amino groups) to increase the compatibility between MWCNTs and PEEK.

2.2.1 Preparation of acid-functionalized MWCNTs

Acid-functionalized MWCNTs with carboxylic groups were prepared in strong mixing acid. p-MWCNTs (3.0 g) were treated in 240 mL of mixing acid of H_2SO_4 and HNO_3 (3/1, v/v) under sonication at 50°C for 2 hours. The supernatant was removed and the sediment was washed by deionized water until neutral. The product was dried in a vacuum oven at 80°C for 24 hours and marked as a-MWCNTs in which hydroxyl and carboxyl groups were grafted on the surfaces of MWCNTs [19], as shown in Fig. 1(a).

2.2.2 Grafting of ethanolamine to MWCNTs

In this grafting process, 0.6 g of a-MWCNTs and 0.2 g of DCC were added into

150 ml of anhydrous ethanol and sonicated in an ultrasound bath at 50°C for 20 minutes. Subsequently, a solution of anhydrous ethanol (150 mL) with ethanolamine (0.6 mL) was added. Then, the solution and a-MWCNTs dispersion were mixed in a flask and the reaction was allowed to proceed under magnetic stirring at 50°C for 10 hours. Finally, the reaction mixture was washed with ethanol and water respectively and dried under vacuum at 80°C for 24 hours to obtain the product marked as e-MWCNTs, and amino groups were grafted on the surfaces of MWCNTs [19], as shown in Fig. 1(b).



NH₂

NH2



(b) Preparation of e-MWCNTs

Fig.1 The schematic views of principles in surface modification of MWCNTs: preparation of (a)a-MWCNTs and (b) e-MWCNTs.

2.3 Fabrication of MWCNT/PEEK composites

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In the preparation process of MWCNT/PEEK composites, p-, a- and e-MWCNTs were mixed with PEEK separately. Pure PEEK (1.92 g) was added into 10 mL of DMF and sonicated for 30 minutes at 30 °C. Then the polymer solution was mixed

with 0.08 g of p-, a- and e-MWCNTs, separately. Each mixture was sonicated for 30 minutes at 30°C and then each product was added into an aluminum mould. The composites were dried at 60°C until a constant weight was achieved.

2.4 Materials characterization

2.4.1 Scanning electron microscopy

The morphology of the different MWCNTs and MWCNTs/PEEK composites was observed with a JSM-6700F scanning electron microscope (SEM, acceleration voltage: $0.5\sim3.0$ kV, beam intensity: $10^{-13}\sim2\times10^{-9}$ A, operated at 10 kV). The samples were coated with gold in an evaporator to avoid charging during electron irradiation.

2.4.2 Fourier transformation infrared (FTIR) spectroscopy

The chemical structures of parent and modified MWCNTs were characterized using a TENSOR 27 Fourier transformation infrared (FTIR) spectrometer. Spectra were recorded at a spectral resolution of 1.5 cm^{-1} , and two scans were collected for each sample in the range of 4000~500 cm⁻¹.

2.4.3 Dynamic mechanical analysis

The dynamic mechanical properties of the different MWCNT/PEEK composites were studied using a NETZSCH-242E dynamic mechanical analyzer (DMA) at a frequency of 1 Hz and each sample was tested at least two times to verify the test repeatability of all samples.

2.4.4 Friction and wear tests

The tribological properties of the composites were evaluated by a POD 2 Pin-on-disc tester. All the friction and wear tests were carried out in a dry sliding condition at the ambient temperature of 24°C. Both a linear speed of 0.0295 m/s and a contact load of 3.929 N on the pin were applied in each test for a duration of one hour. The morphology of the worn surfaces of the material samples and the scratching depth on these worn surfaces were observed with a VHX-1000 optical microscope.

3. Results and discussion

3.1 The sole-dispersibility of MWCNTs

The morphology of MWCNTs was observed by SEM. Fig. 2 shows SEM micrographs of p-MWCNTs, a-MWCNTs and e-MWCNTs. From Fig. 2(a), it can be seen clearly that p-MWCNTs were accumulated loosely with large tube gaps and each nanotube had a uniform pipe diameter. Fig. 2(b) shows that after the acid treatment, a-MWCNTs became shorter and denser, indicating that carboxyl groups were grafted on the surfaces of nanotubes and the hydrogen bonding formed by carboxyl groups resulted in the agglomeration of the nanotubes [20]. As shown in Fig. 2(c), compared with a-MWCNTs, the sole-dispersibility of e-MWCNTs was obviously improved and the e-MWCNTs showed no agglomeration owing to grafting of amino groups on the surfaces of nanotubes [21].



Fig. 2 SEM observations of different MWCNTs: (a) p-MWCNTs, (b) a-MWCNTs, (c) e-MWCNTs.

3.2 The chemical groups on surfaces of the MWCNTs

The identification of the chemical groups onto the MWCNT surfaces was conducted through FTIR spectroscopy. The spectra of p-, a- and e-MWCNTs are compared in Fig. 3. It can be seen that p-MWCNTs show no relevant features except the band at 3430 cm⁻¹ and 1560 cm⁻¹. The band at 1560 cm⁻¹ is attributed to the C=C stretching of the main structures of the MWCNTs [22] and the band around 3430 cm⁻¹ is the O-H stretching owing to the preparation process of p-MWCNTs. Fig. 3 also shows that a-MWCNTs present a broad absorption centred at 3430 cm⁻¹ assigned to the O-H stretching of the carboxylic group, and a band at 1640 cm⁻¹ corresponding to

the C=O stretching vibration [13], which has an agreement with the preparation of a-MWCNTs as shown in Fig. 1(a). The C-H stretching vibrations occur around 2920 cm⁻¹ and 2850 cm⁻¹, and the band around 1410 cm⁻¹ is ascribed to C-H bending of methylene groups. Regarding the spectra of e-MWCNTs, the band at 3380 cm⁻¹ corresponds to asymmetrical stretching vibrations of N-H group. Therefore, it is suggested that the amino groups (-NH₂) of ethanolamine have been grafted on the surfaces of MWCNTs, as shown in Fig. 1(b).



Fig. 3 FTIR spectra of p-MWCNTs, a-MWCNTs and e-MWCNTs.

3.3 The dispersibility of MWCNTs in PEEK

SEM was also employed to observe the dispersibility of MWCNTs in PEEK. Achieving a good distribution of carbon nanotubes in PEEK matrix is a commonly difficult task, because p-MWCNTs have a strong tendency to gather and form bundles [2]. Fig. 4 shows a comparison of typical micrographs of p-MWCNT/PEEK, a-MWCNT/PEEK and e-MWCNT/PEEK composites with a concentration of 4 wt% MWCNTs. In Fig. 4, MWCNTs appeared as bright spots, as indicated by dash arrows. It can be seen in Fig. 4(a) that p-MWCNT/PEEK composites showed an agglomeration of p-MWCNTs, the domain size of the dispersed phase was large and there were small regions where p-MWCNTs agglomeration could be observed as marked by a dash circle. As shown in Fig. 4(b), a-MWCNTs were also agglomerated in PEEK matrix but dispersed better in PEEK than p-MWCNTs in PEEK, probably owing to grafting of carboxyl groups (-COOH) on the surfaces of MWCNTs. As shown in Fig. 4(c), e-MWCNT/PEEK displayed an improved dispersion of the reinforcement phase. Therefore, it is suggested that a reaction between amino groups (-NH₂) on the surfaces of e-MWCNTs shown in Fig. 1(b) and carbonyl groups (-C=O) of PEEK may yield an interaction between e-MWCNTs and PEEK.



Fig. 4 SEM observations of different MWCNT/PEEK composites: (a) p-MWCNT/PEEK, (b) a-MWCNT/PEEK, (c) e-MWCNT/PEEK.

In order to calculate the interaction energy of all complexes formed between functional groups on the surfaces of MWCNTs and PEEK, a numerical simulation was carried out with an Ab initio quantum chemistry package, $Dmol^3$ code. The present level of calculation, density functional theory (GGA-PBE)/double numeric polarized DFT (GGA-PBE)/DNP, was used to optimize the geometries of all compounds, and TS method DFT-D for correction was used for dispersion correction. Interaction energy (ΔE) was calculated from the following equation:

$$\Delta E = E_{(MWCNT/PEEK)} - (E_{PEEK+} E_{MWCNTs})$$
(1)

The best optimized structures of finite PEEK, a-MWCNTs, e-MWCNTs, a-MWNCT/PEEK and e-MWCNT/PEEK composites are presented in Fig. 5. Table 1 shows a list of calculated interaction energy for all complexes formed between PEEK

and the functional groups on the surfaces of MWCNTs. It can be seen that a-MWCNT/PEEK had higher binding energy: ($\Delta E(e-MWCNT/PEEK$) > $\Delta E(a-MWCNT/PEEK$)). Accordingly, it can be concluded that the interaction between the –NH₂ on surfaces of e-MWCNTs and the -C=O of PEEK is much stronger than the interaction between the –COOH on surfaces of a-MWCNTs and the –C=O of PEEK [23].



Fig. 5 Optimized structures of finite PEEK and MWCNT/PEEK composites: (a) PEEK, (b) a-MWCNTs, (c) e-MWCNTs, (d) a-MWCNT/PEEK and (e) e-MWCNT/PEEK.

Molecules	<i>E</i> (a.u)	<i>∆E</i> (a.u)	ΔE^{a} (kcal mol ⁻¹)
PEEK	-1035.8545997	_	_
a-MWCNTs	-420.494824	-	-
e-MWCNTs	-554.3342676	_	_
a-MWCNT/PEEK	-1456.3448938	0.020331	12.75777
e-MWCNT/PEEK	-1590.2159633	0.027096	17.00299

 Table 1 Summary of the binding energies of complexs at GGA/PBE (DFT-D correction) level.

a $1a.u = 627.5094 kcalmol^{-1}$

3.4 The dynamic mechanical properties of MWCNT/PEEK composites

The main goal of surface modifications of MWCNTs is to improve the mechanical properties of the MWCNT/PEEK composites. These properties of the composites depend on many factors, such as the compatibility between MWCNTs and PEEK. The effects of surface modifications of MWCNTs on the dynamic mechanical properties of MWCNT/PEEK composites have been investigated by DMA. Fig. 6 shows the temperature dependence of the storage modulus E' (Fig. 6(a)) and tan δ (Fig. 6(b)) of pure PEEK and different types of MWCNT/PEEK composites with an identical MWCNTs concentration of 4 wt% at a frequency of 1 Hz. As can be seen in Fig. 6(a), storage modulus E' decreased slowly and progressively with temperature, showing a very sharp drop in the temperature range between 80 and 100°C. The fall of storage modulus was attributed to an energy dissipation phenomenon involving cooperative motions of the polymer chains [24]. From Fig. 6(a), it can be seen clearly that the incorporation of MWCNTs induced an obvious increase in storage modulus E' of the matrix at a given temperature below about 80°C. The increase of storage modulus E' of e-MWCNT/PEEK composites was most pronounced. At 25°C, the value of storage modulus E' of the e-MWCNTs composites was the highest and approximately 83.78% higher, while the value of storage modulus E' of p-MWCNT/PEEK and a-MWCNT/PEEK composites was 24.61% and 42.41% higher, respectively, than that of pure PEEK, respectively. It appears that such a significant increase in the value of storage modulus E' of the e-MWCNT/PEEK composites corresponds to an improved dispersibility of e-MWCNTs in PEEK as shown in Fig.4. Therefore, the modulus increase of e-MWCNT/PEEK composites should be attributed to the improved interfacial adhesion strength and stress transfer ability between the e-MWCNTs and PEEK [15].



Fig. 6 DMA spectra of pure PEEK and different types of MWCNT/PEEK composites (4% MWCNTs) at a frequency of 1 Hz: (a) Storage modulus E' versus temperature; (b) tanδ versus temperature.

Fig. 6(b) shows tan δ curves versus temperature of pure PEEK and different types of MWCNT/PEEK composites (4% MWCNTs) at a frequency of 1 Hz. It can be seen that an increase in glass transition temperature (T_g) was observed in all MWCNT/PEEK composites, owing to the strong restrictions on polymer chain mobility caused by the incorporation of MWCNTs. Fig. 6(b) also shows that glass transition temperature T_g of pure PEEK was 133°C and the T_g of p-MWCNT/PEEK, a-MWCNT/PEEK and e-MWCNT/PEEK composites was increased by about 1, 2 and 7°C, respectively. The increase of e-MWCNT/PEEK composites' T_g is considerably higher than that of the others. This phenomenon was probably related to the more homogeneous distribution of e-MWCNTs in PEEK [13]. Moreover, a diminution of the height of tan δ peak from MWCNT/PEEK composites was observed because of the strong MWCNT-polymer interactions. The tan δ peak value of e-MWCNTs was least. It suggests that the interactions between e-MWCNTs and PEEK were stronger than those in p-MWCNT/PEEK and a-MWCNT/PEEK composites.

3.5 The macro friction and wear behaviours of MWCNT/PEEK composites

Fig. 7 presents the friction coefficient of pure PEEK and MWCNT/PEEK composites tested at a sliding velocity of 0.0295 m/s and normal load of 3.929 N. As shown in Fig. 7, the friction coefficient of a-MWCNT/PEEK was higher than that of pure PEEK, the friction coefficient of p-MWCNT/PEEK became higher than that of pure PEEK after about 2290 seconds during the test. The friction coefficient of e-MWCNT/PEEK composites was the least and reduced by about 12% compared with that of pure PEEK.



Fig. 7 Friction coefficient versus time of MWCNT/PEEK composites (4% MWCNTs) at the load of 3.929 N and sliding velocity of 0.0295 m/s.

Fig. 8 shows the morphology of worn surfaces of the material samples (Fig. 8(I)) and the scratching depth (Fig. 8(II)) on these worn surfaces of pure PEEK and MWCNT/PEEK composites. As shown in Figs. 8(I)-(II), the scratching depth on PEEK sample surfaces was the largest and the maximum depth was 95.92 µm. After adding MWCNTs into PEEK matrix, the scratching depth of MWCNT/PEEK composites was reduced considerablyly. The scratching depth of e-MWCNT/PEEK composites was 18µm and was reduced by about 81% compared with that of pure PEEK.



Fig. 8 The morphology of the wear surfaces (I) and the scratching depth (II) of pure PEEK and MWCNT/PEEK composites: (a) pure PEEK, (b) p-MWCNT/PEEK, (c) a-MWCNT/PEEK and (d) e-MWCNT/PEEK.

Table 2 shows both weight change (Δm) and volume change (ΔV) of pure PEEK and MWCNT/PEEK samples before and after friction tests. F_N was 3.929 N and L was 106.2 m in the friction tests. The specific wear rate (W_s) is calculated by following equation:

$$W_s = \frac{\Delta m}{\rho F_N L} \text{ or } \frac{\Delta V}{F_N L} \left(\frac{mm^3}{Nm}\right) \tag{2}$$

where ΔV is a volume change of the test samples over a period of one hour test, F_N is the normal load and L is the total sliding distance [25]. It can be seen from Table 2 that the specific wear rate W_s of a-MWCNT/PEEK composites was the highest in all samples owing to the agglomeration of a-MWCNTs in PEEK matrix. The specific wear rate W_s of e-MWCNT/PEEK composites was the lowest in all test samples. It suggests that the improved dispersibility of e-MWCNTs in PEEK could reduce the specific wear rate of MWCNT/PEEK composites and improve the tribological properties of MWCNT/PEEK composites significantly.

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Test samples	Δm (g)	$\Delta V (cm^3)$	W _s (mm ³ /Nm)
Pure PEEK	0.0008	0.001486	1.486×10^{-3}
p-MWCNT/PEEK	0.0003	0.000557	5.573×10 ⁻⁴
a-MWCNT/PEEK	0.0011	0.002043	2.044×10 ⁻³
e-MWCNT/PEEK	0.0002	0.000371	3.716×10 ⁻⁴

Table 2 The W_s of pure PEEK and MWCNT/PEEEK composites obtained from friction tests.

The SEM images of worn surfaces after testing and cleaning are shown in Fig. 9. It can be seen in Fig. 9(a) that the wear scar of pure PEEK was very deep and wide after its wear test. It illustrates that the surface of pure PEEK had very serious wear and material loss. From Figs. 9(b) and 9(c), it can be seen that the wear scars of p-MWCNT/PEEK and a-MWCNT/PEEK composites were shallower than the wear scar of pure PEEK. The worn surfaces of p-MWCNT/PEEK and a-MWCNT/PEEK composites were smoother than that of pure PEEK. However, p-MWCNTs and a-MWCNTs were not dispersed well within the PEEK matrix and some MWCNTs were exposed to the outside of the PEEK matrix after wear tests. It can be seen clearly in Fig. 9(d) that the worn surface of e-MWCNT/PEEK composites was smoothest, no

abrasion trace of agglomerates was seen and e-MWCNTs showed the best dispersibility in PEEK matrix.



Fig. 9 Typical wear scars of pure PEEK and MWCNT/PEEK composites: (a) pure PEEK, (b) p-MWCNT/PEEK, (c) a-MWCNT/PEEK, (d) e-MWCNT/PEEK.

The testing results shown in Fig. 9 reflect an important material property of MWCNT/PEEK composites that is a self-lubricating capability. Under the identical testing conditions, a reduction of friction coefficient may be resulted from a boundary lubrication behaviour on the contact surfaces of the MWCNT/PEEK composites without any external lubricant [26]. Therefore, it is suggested that this observed lubrication behaviour of the MWCNT/PEEK composites was yielded from materials in contact and may be called as self-lubricating. With such behaviour, the contact surfaces of composites could be protected significantly and the friction coefficient was reduced obviously [27]. It is well known that carbon is a kind of lubricant. However, as shown in Fig. 9, with identical percentage of multi-walled carbon nanotubes, different types of MWCNT/PEEK composites have a different level of self-lubricating capability. The key difference among these three types of

MWCNT/PEEK composites is a different approach in surface modifications of MWCNTs. As shown in Fig. 4, these three types of MWCNTs have different dispersibility and compatibility in MWCNT/PEEK composites. When p-MWCNTs and a-MWCNTs were agglomerated in PEEK matrix, as shown in Figs. 9(b) and (c), it was difficult for MWCNTs within the composites to be smeared widely and uniformly between the contact surfaces in sliding so that these two types of composites showed a poorer self-lubricating capability. The compatibility between PEEK and p-MWCNTs or a-MWCNTs appears to be much lower than that between e-MWCNTs and PEEK so that it is difficult for the p-MWCNTs and a-MWCNTs to be embedded into the matrix [28], [29], [30] and [31]. The better compatibility and interfacial adhesion [32] between e-MWCNTs and PEEK lead to a better opportunity for MWCNTs within the composites to be smeared on the contact surfaces of e-MWCNT/PEEK composites during the sliding test so that e-MWCNT/PEEK composites have the best self-lubricating capability among pure PEEK and three composites. This is in agreement with an SEM image of the worn surfaces on e-MWCNT/PEEK composites shown in Fig. 9(d). As a result, the friction coefficient of e-MWCNT/PEEK composites was lowest among those of pure PEEK, p-MWCNT/PEEK, a-MWCNT/PEEK and e-MWCNT/PEEK composites.

4. Conclusions

In the present work, surface modifications of MWCNTs, and the morphology, dynamic mechanical and tribological properties of MWCNT/PEEK composites have been investigated. Morphological observations show that the sole-dispersibility of MWCNTs and the compatibility between MWCNTs and PEEK were improved significantly when MWCNTs were modified by grafting ethanolamine. DMA measurements indicate that the filling of e-MWCNTs to PEEK leads to an obvious enhancement in the storage modulus of the composites, owing to an improved interfacial adhesion and stress transfer ability between e-MWCNTs and PEEK matrix. Moreover, an increase in the glass transition temperatures of the composites is

produced because of the chain motion restriction imposed by the strong interfacial interactions between MWCNTs and PEEK matrix. The sliding tests show that the tribological properties of e-MWCNT/PEEK composites were better than pure PEEK, p-MWCNT/PEEK composites and a-MWCNT/PEEK composites although all three MWCNT/PEEK composites have self-lubricating capabilities. In particular, e-MWCNT/PEEK composites have the best self-lubricating capability due to dispersibility of MWCNTs in PEEK matrix and the compatibility between MWCNTs and PEEK. This study sets the way towards the choice of proper MWCNTs' modification routes to enhance specific properties of MWCNT/PEEK composites.

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